

108/114/12/R8-4

**UMKHOMAZI WATER PROJECT**  
**MODULE 3 – POTABLE WATER MODULE**

**Detailed Feasibility Study**  
**Geotechnical Investigation Report – Volume 4**  
**(Mapstone Dam Crossing)**

**Revision 1**

**October 2015**



**Planning Services**  
**Engineering & Scientific Services**  
**Umgeni Water**

Prepared By:

***Knight Piésold***  
**CONSULTING**

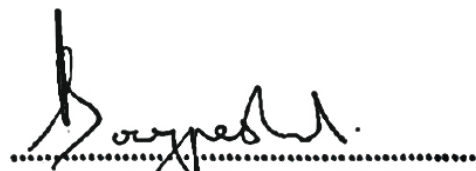
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**uMkhomazi Water Project**

**Detailed Feasibility Study - Geotechnical Investigation  
Report – Volume 4 (Mapstone Dam Crossing)**

*Report No. 108/114/12/R8-4*

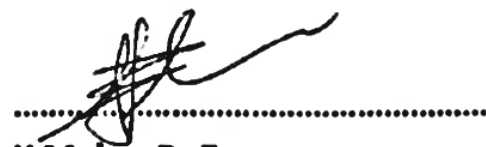
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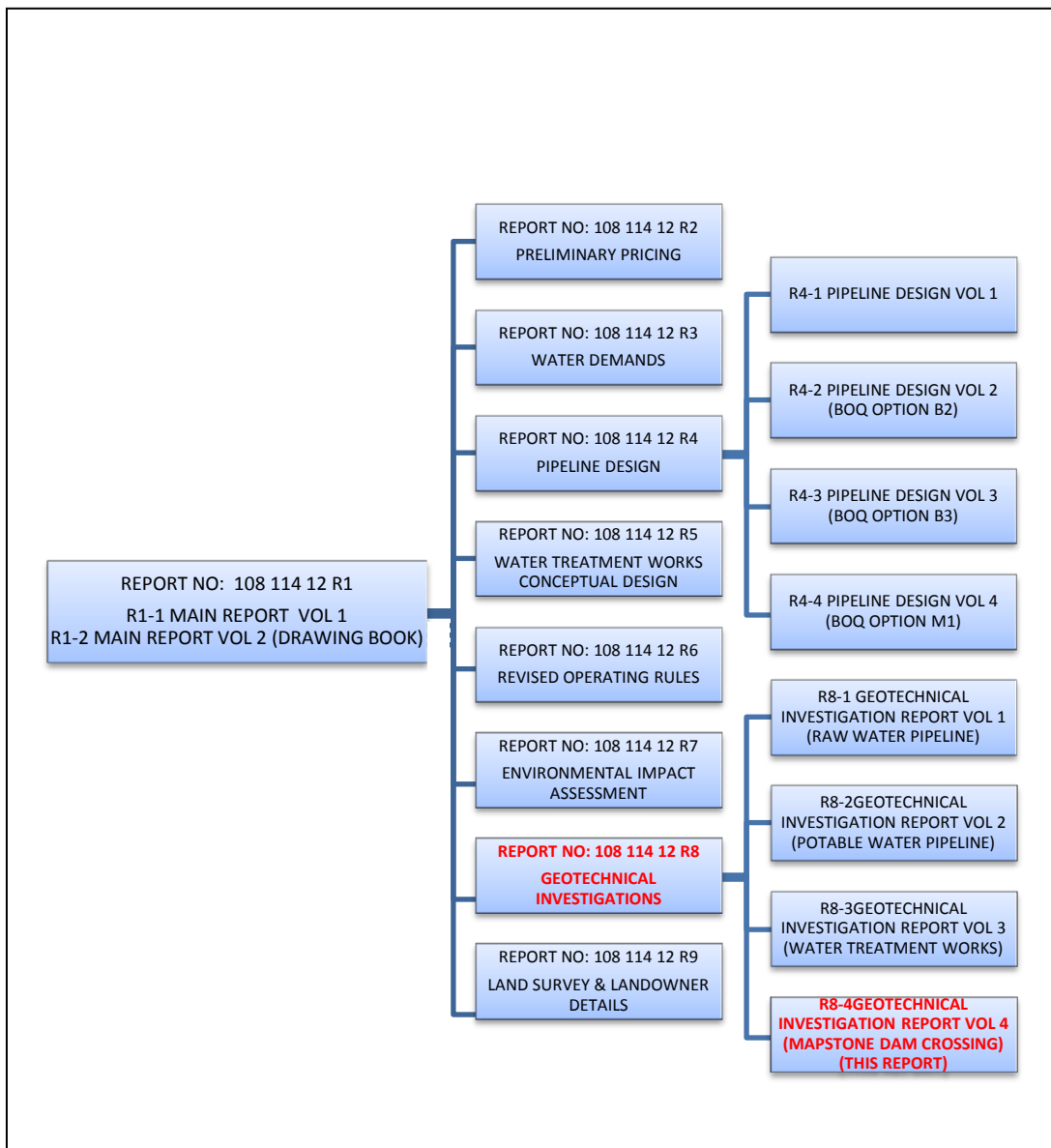
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# UMKHOMAZI WATER PROJECT

## MODULE 3 – POTABLE WATER MODULE

### Structure of Suite of Reports



# DOCUMENT CONTROL SHEET

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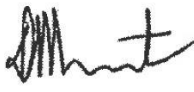
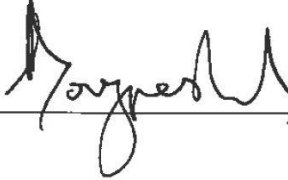

**PROJECT:** uMkhomazi Water Project, Potable Water Module

**PROJECT ASSIGNMENT:** uMkhomazi Water Project P/A No: 30300413/01

**TITLE:** Detailed Feasibility Study – Geotechnical Investigation Report – Volume 4 (Mapstone Dam Crossing), Revision 1

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## 1. Introduction

Knight Piésold (KP) was appointed by Umgeni Water (UW) to perform geotechnical investigations for the proposed Umkhomazi Water Project Phase 1 (uMWP-1). These investigations were undertaken in March 2014. This appointment was extended in November 2014 to include a drilling investigation at the Mapstone Dam to determine the ground conditions along the alignment where the route intersects the dam.

The potable pipeline route intersects the Mapstone Dam between CH 5380 and CH 5510. An alternate route around Mapstone Dam was investigated but although technically feasible, initial cost estimates indicated that crossing Mapstone Dam would be a cheaper option. Various options were proposed to cross Mapstone Dam including a suspension bridge, conventional steel bridge or pipe on concrete piers and laying the pipe on the bed of the dam. To support these options, Umgeni Water decided to carry out geotechnical investigations of the dam basin geology. This led to a drilling investigation in the Mapstone Dam to determine soil profile and bedrock conditions.

This report provides recommendations on founding conditions for the bridge footings and for mass concrete cradles to anchor the pipe along the floor of the dam, The report includes all supporting documentation.

## 2. Existing Information

The following information was provided to the Geotechnical team:

- Longitudinal topographic section showing the existing and proposed full supply level of Mapstone Dam.
- Design report of the Mapstone Dam by Bradford, Conning & Partners, dated January 1994 [1].

The proposed pipeline route intersects the dam at a position where the basin is relatively narrow, viz. approximately 140m between existing full supply levels. The results of the existing test pits excavated on dry ground adjacent to the dam, revealed the following [2]:

- Test pit PL20 was excavated on the flat slope west of the dam, approximately 23m from the edge of the water line. It was excavated to a depth of 3,1m in firm to stiff residual tillite soil without having reached TLB refusal. The residual tillite comprised clayey silt.
- Test pit PL21 was excavated on the steep slope to the east of the dam, approximately 25m from the edge of the water line. PL21 refused on tillite bedrock at a depth of 0,5m.

It follows from the above that variable ground conditions can be expected in the basin of the dam. According to the Bradford, Conning & Partners dam design report, conditions in the basin are relatively variable. TLB refusal was often encountered on alluvial boulders at depths of about 2m. It was therefore recommended to drill rotary cored boreholes to distinguish between boulders and bedrock below the water.

### 3. Method of Investigation

Five rotary cored boreholes at approximately 30m intervals were drilled to depths of between 9m and 13,3m below the dam ground level at the Mapstone dam. Standard Penetration Tests (SPT's) were done at 1,5m intervals where possible to determine the soil consistencies. A total of nine SPT tests were done. Four boreholes were drilled from a barge (BH2 to BH5), while BH1 was drilled from natural ground to the west of the water edge. The water depths at the various borehole positions are given below:

- BH1 – natural ground level
- BH2 – 1,95m
- BH3 – 3,85m
- BH4 – 8m
- BH5 – 1,25m

Access to the dam was from district road D360 which runs past the Mapstone Farmstead located towards the west of the dam. The barge was floated into position and secured to the shore by means of ropes and cables. The barge used had dimensions of approximately 4m x 3m. Drilling of the boreholes positioned over water was performed from the barge. The boreholes were set out by an engineering geologist by means of a small canoe and a handheld GPS. Borehole positions were marked by means of small buoys fixed to the bottom of the dam with fishing line and rock boulders.

All drilling procedures were conducted in accordance with the Standard Specification for Subsurface Investigation published by SANRAL Secretariat (2012 Edition). Water from the dam was used for drilling purposes (cooling of drill stem and removal of drill cuttings). All return water was collected in plastic containers on the barge and was circulated in some instances. Some drill water might have spilled into the dam (leakages at the intersection of the casing with the bed of the dam and from the top of the casing onto the floor of the barge). Drilling water carries sediment but is non-toxic. All drilling additives used were bio-degradable and non-toxic.

Drill samples were collected from core barrels in a cylindrical form and were placed in core boxes of 1,5m in length.

Borehole logs and core photographs are provided in Appendices A and B respectively.

No laboratory testing was done on the core samples.

### 4. Site description

The proposed potable water pipeline is situated in the uMkhomazi River Catchment and is located between Umlaas Road and Baynesfield, in the Natal Midlands of the KwaZulu-Natal Province. The Midlands are characteristic of undulating and hilly terrain intersected by a well-developed dendritic drainage system comprising well-defined drainage features. The steepest area on the pipeline route occurs just east of the Mapstone Dam, which has an approximate slope of 24° towards the west. The Mapstone Dam wall occurs approximately 1,4km south-west of the pipeline route intersection. The



dam itself has a meander shape with a length of approximately 3,1km. The pipeline route passes Hopewell Village along its northern boundary.

The locality of the site is shown in Figure 1 at the back of the report.

## 5. Geology

The regional geology of the area is described in detail in the potable pipeline geotechnical report [2], and is not repeated here. For the purpose of this report, the site geology of the pipe crossing is described below.

The entire proposed pipe bridge crossing is underlain by tillite of the Dwyka Group, Karoo Supergroup. The contact with the overlying strata of the Pietermaritzburg Formation (shale, siltstone and sandstone) occurs to the west of the Mapstone Dam. A north-northwest striking fault runs along a portion of the river within Mapstone Dam and it intersects the bridge site in the vicinity of BH5.

A layer of transported soil covers most of the area, particularly to the east of the dam, where it attains a thickness of up to 2m in BH4 and BH5. Elsewhere the transported soil cover is generally 0,3m thick. The transported soil layer is, however, underlain by clayey residual tillite soil to depths of up to 7,5m. This is the result of chemical decomposition associated with the hot and humid climate of the region. The eastern portion of the dam is, however, characterised by a steep valley bank and scattered tillite outcrops.

Although covered by water, alluvial terraces occur in the vicinity of the submerged river channel, but these are expected to be of limited extent only. It is likely that both BH4 and BH5 were drilled into such an alluvial terrace, hence the 2m thick transported soil cover encountered along the eastern portion of the dam.

## 6. Drilling Results

Since most of the pipe crossing was inundated with water at the time of the investigation, the drilling results are the sole source of information on the subsoil conditions, i.e. no interpretative assistance possible from surface features, satellite imagery, etc.

Results of the five boreholes drilled along the pipe bridge are summarised in Table 1 below, while Figure 3 provides a geological longitudinal section along the alignment.

**Table 1: Summary of Rotary Cored Drilling**

Borehole No.	Total Depth (m)	Depth of Layers (m) - (m)			
		Transported	Residual Tillite Soil	Tillite Bedrock	
		Colluvium and Alluvium		Highly weathered	Slightly weathered to unweathered
BH1	13,3	0 - 0,4	0,4 - 6,4	6,4 - 7,5	7,5 - 13,3
BH2	12,0	0 - 0,3	0,3 - 4,3	4,3 - 6,2	6,2 - 12,0
BH3	9,0	0 - 0,3	0,3 - 3,8	-	3,8 - 9,0
BH4	9,09	0 - 2,94	-	-	2,94 - 9,09
BH5	9,65	0 - 2,0	2,0 - 3,1	3,1 - 4,4	4,4 - 9,65

Standard Penetration Tests (SPT's) were conducted in the soil layers overlying rock to determine soil consistencies. The results are indicated on the borehole core logs, but are summarised in Table 2 below.

**Table 2: Summary of Standard Penetration Test (SPT) Results**

Borehole No.	Depth (m) - (m)	Material Description	Origin	Uncorrected SPT N-Value	Soil Consistency
BH1	1,5 - 1,95	Sandy clay	Residual Tillite	7	Firm
	3,0 - 3,45	Sandy silt	Residual Tillite	18	Very Stiff
	4,5 - 4,95	Sandy silt	Residual Tillite	49	Very Stiff
	6,0 - 6,15	Sandy silt	Residual Tillite	Refusal	Very Stiff / Boulders
BH2	1,5 - 1,95	Sandy clay	Residual Tillite	4	Soft
	3,0 - 3,45	Sandy clay	Residual Tillite	15	Stiff
BH3	1,5 - 1,95	Silty clayey sand	Residual Tillite	13	Medium Dense
BH4	1,5 - 1,95	Sandy clay	Residual Tillite	8	Firm
BH5	1,5 - 1,95	Sandy clay	Alluvium	16	Stiff

It follows from the above that the consistency of the residual tillite generally improves with depth, but varies from soft to firm at depths above 2m to stiff and very stiff with depth.

Highly weathered tillite bedrock occurs below the residual tillite soil. This boundary is not considered to be well-defined, but rather represents a gradual transition with depth. The highly weathered tillite rock interface was not encountered in BH3 and BH4, which is in accordance with the irregular nature of the chemically weathered rock mass. This zone should be seen as transition between residual soil and rock. It may therefore contain substantial zones of relatively soft soil within the soft rock.

The highly weathered rock (where present) grades relatively abruptly to slightly weathered and unweathered rock at depths varying below original ground surface between 7,5m (BH1) and 3m (BH4). The shallow depths are possibly related to the original river channel, where the soft, weathered rock/residual soil have been removed by river erosion. Figure 3 provides an interpretative sound rock line along the bridge site, based on the drilling results. The sound rock comprises slightly weathered to unweathered medium jointed hard rock tillite.

## 7. Geotechnical Considerations

### 7.1 Bridge Foundation

Pipe bridge foundations will for as long as the Mapstone Dam exists not be subjected to scouring caused by river flow. Erosion is usually the most critical foundation parameter for a bridge over river scenario. For the uMkhomazi study, the safe bearing capacity of the foundations is the main concern.

SPT results indicated that the upper 2m to 3m of the soil horizon comprise soft to firm residual soil with a safe bearing capacity of about 80kPa. The stiff to very stiff ( $N > 15$ ) soil encountered below a depth of 3m in most of the boreholes, will have a safe bearing capacity of at least 150kPa, which is not considered suitable for a large sensitive pipe bridge structure. This is furthermore complicated by the variable thickness of the compressible layer. Therefore, it is recommended that the foundations for the bridge piers be placed on sound rock. Sound rock level is indicated in Figure 3. According to published data on the strength of tillite in KwaZulu-Natal, unweathered tillite has average Uniaxial Compressive Strength (UCS) values of 150MPa [3]. The following rock mass properties can be used for both founding or rock anchoring, assuming the UCS of the sound tillite is at least 100MPa and the minor principle stress amounts to less than 2MPa, i.e. shallow overburden conditions:

Ultimate Bearing Capacity	:	7MPa - 10MPa
Rock Mass Deformation Modulus	:	18GPa
Average Rock Mass Shear Strength	:	Cohesion: 1,6MPa
	:	Friction: 55°
Tensile Strength	:	270kPa

The maximum water depth along the pipe bridge will amount up to 10m at about ch 270m (old river channel). It decreases gradually on the western bank, but the eastern bank is relatively steep (less than 40m long). It follows that it will be possible to provide pier supports along the length of the pipe bridge in areas of relatively shallow water (less than 5m) by means of a piling rig on a barge. Piles should be founded in the sound tillite zone as indicated in Figure 3, where up to 5MPa end bearing pressures can be used. Limited socketing of less than say 0,5m into sound rock will be required to counter for lateral stress caused by wind.

For suspension bridge options, a combination of concrete anchor blocks and rock anchors are proposed. Sound tillite rock has good shear strength properties and will provide suitable material for the installation of rock anchors. It has a dry density of between 2500kg/m<sup>3</sup> and 2650kg/m<sup>3</sup> [3].

## 7.2 Pipe Anchoring

A syphon type dam crossing can also be considered whereby the pipe is anchored to the floor of the dam by means of concrete cradles. The pipe trench should be excavated into at least highly weathered tillite and/or doweled into sound tillite rock. This option will, however, require emptying the dam for a considerable time, which may not be acceptable for the neighbouring farming community. Excavations to highly weathered rock will take place in complete saturated conditions and flat excavation slopes will be required, probably 1:2 (V:H). Dewatering will be required during construction. The expected minimum excavation level for founding of the concrete anchoring cradles is indicated as the soil-rock interface level in Figure 3. The safe bearing capacity for highly weathered tillite is in the region of 800kPa.

## 8. Conclusions and recommendations

A geotechnical investigation was conducted for a pipe crossing over the Mapstone Dam as part of the Umkhomazi Water Project (Potable Water Pipeline). The investigation comprised the drilling of five rotary cored boreholes in November and December 2014. Four of the boreholes were drilled from a barge in the dam.

The entire site is underlain by tillite of the Dwyka Group, Karoo Supergroup, which is characterised by a well-developed mantle of chemical decomposed residual soil. The thickness of this mantle is somewhat variable, which is typical of a chemical decomposed profile, although erosion caused by the river also contributed to thinner soil horizons in the lower-lying river channel areas.

SPT's conducted in the soil horizons as part of the drilling process, indicated that the upper 2m to 3m of the soil profile generally comprises soft to firm clayey soils, which are not considered suitable for foundations for a bridge structure. Where the residual soils extend with depths (up to 6m in places), the residual soil horizon transitions to sandy silt/silty sand with a stiff to very stiff (or medium dense where sandier) material. According to the (limited) SPT results in this horizon, the lower portion of the residual tillite has a safe bearing capacity of about 150kPa.

Slightly weathered to unweathered tillite rock (referred to as sound tillite) occurs at a relatively shallow depth along the pipe bridge alignment, from 7,5m depth at BH1 (drilled from dry ground on western bank of dam) to about 3m to 4m in the old river section area and eastern bank. The eastern bank is steep and characterised by scattered tillite outcrop.

It is recommended that foundations for the bridge piers or suspended bridge abutments be taken down to sound tillite. Rock anchoring for suspended structures can be done in the sound rock, which has good foundation properties, viz.

Ultimate Bearing Capacity	:	7MPa - 10MPa
Rock Mass Deformation Modulus	:	18GPa
Average Rock Mass shear strength	:	Cohesion: 1,6MPa
	:	Friction: 55°

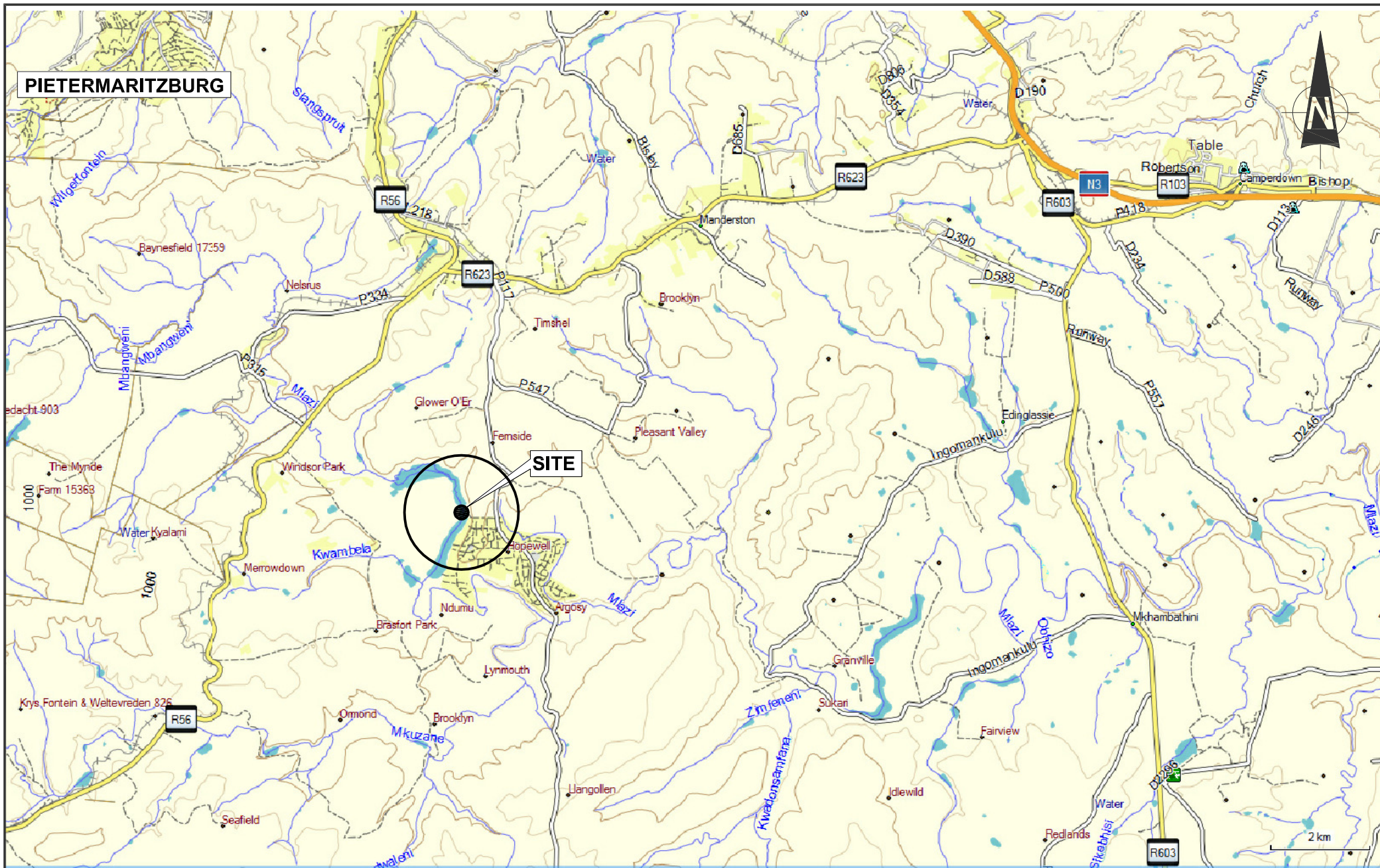
It is considered feasible to construct the foundations of the bridge piers from a barge in about 5m deep water using a small piling rig.

Pipe trench excavations along the dam floor will be required for the option to fixing the pipe to the floor of the dam. Concrete cradles will have to be provided, which must be founded on at least highly weathered tillite rock, using 800kPa bearing capacity. The trench excavation will take place in fully saturated clayey soils material. Flattening of cut slopes to at least 1:2 (V:H) will be required in the saturated soils, while the area must be dewatered during construction.

## 9. References

- [1] Umlaas Irrigation Board (1994). Mapstone Dam Final Design Report. Report by Bradford, Conning & Partners.
- [2] Umgeni Water (2014). Umkhomazi Water Project Module 3 - Potable Water Modules. Detailed Feasibility Study. Geotechnical Investigation Report by Knight Piésold, Report No. 108/114/12/R6.
- [3] Brink, A.B.A. (1980). Engineering Geology of Southern Africa, Volume 3. The Karoo Sequence. Building Publications, Pretoria.

**Figure 1: Locality Map**



**PIETERMARITZBURG**

**SITE**

***Knight Piésold***  
CONSULTING

**UMKHOMAZI WATER PROJECT - MAPSTONE DAM  
GEOTECHNICAL INVESTIGATION**

LOCALITY PLAN

PROJECT NO: 30300413/01  
FIGURE NO 1  
SCALE N.T.S.

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Figure 2: Site Plan

9/3/2013



WILLIAM MAPSTONE FARM

CH5100 CH5150 CH5200 CH5250 CH5300 CH5350 CH5400 CH5450 CH5500 CH5550 CH5600 CH5650 CH5700 CH5750 CH5800 CH5850

BH1 BH2 BH3 BH4 BH5

MAPSTONE DAM

POTABLE PIPELINE

HOPEWELL

150 m

Image © 2014 CNES / Astrium

Google

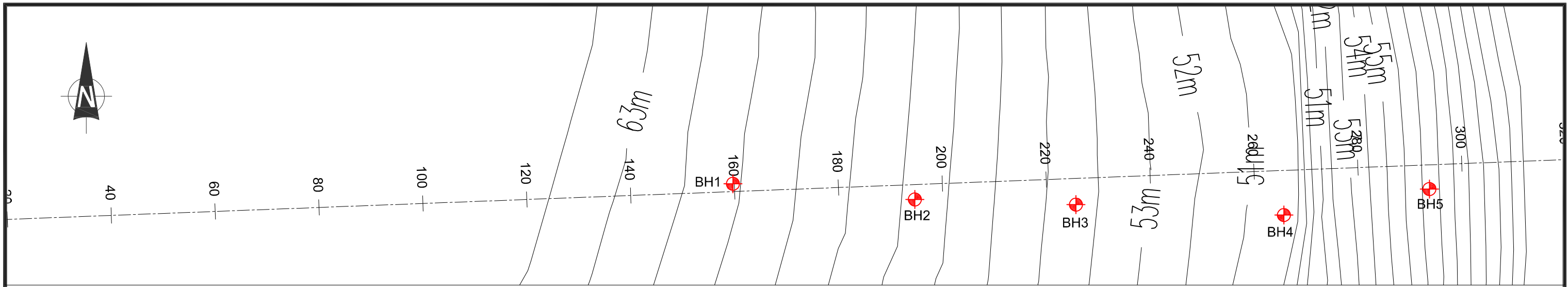
***Knight Piésold***  
CONSULTING

**UMKHOMAZI WATER PROJECT - MAPSTONE DAM**  
**GEOTECHNICAL INVESTIGATION**  
 SITE PLAN SHOWING BOREHOLE POSITIONS

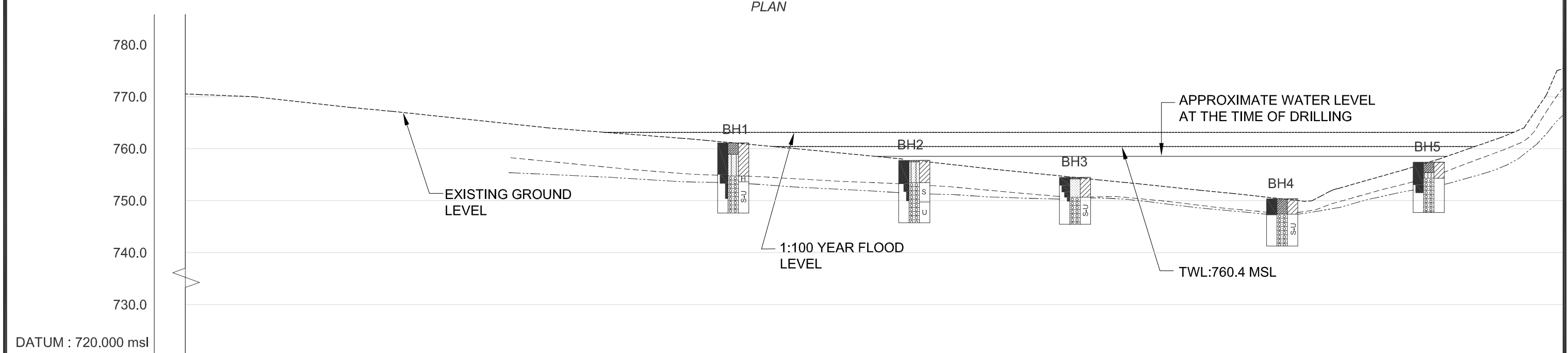
PROJECT NO: 30300413/01  
 FIGURE NO 2  
 SCALE N.T.S.

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Figure 3: Longitudinal Geological Section



PLAN



PEG DISTANCE (m)	GROUND LEVEL (m)
0.000	772.943
60.000	770.298
80.000	768.614
100.000	766.560
120.000	764.444
140.000	762.761
160.000	761.096
180.000	759.205
200.000	757.145
220.000	755.027
240.000	753.002
260.000	750.930
280.000	753.415
300.000	759.555
320.000	775.604

GEOLOGICAL LONGITUDINAL SECTION

**LEGEND:**

<p><b>BOREHOLE LEGEND</b></p> <p>RQD</p>	<p><b>MATERIAL LEGEND</b></p> <p>WEATHERING GRADE</p> <p>SOILS AND BOULDERS</p> <p>C COMPLETELY WEATHERED</p> <p>H HIGHLY WEATHERED</p> <p>M MODERATELY WEATHERED</p> <p>S SLIGHTLY WEATHERED</p> <p>U UNWEATHERED</p>	<p><b>RQD LEGEND</b></p> <p>&lt;25</p> <p>25 - 50</p> <p>51 - 75</p> <p>76 - 90</p> <p>91 - 100</p>	<p><b>BOREHOLE MATERIAL LEGEND</b></p> <p>CLAY - SILT</p> <p>SAND</p> <p>CLAY</p> <p>SILT</p> <p>TILLITE</p>	<p><b>INTERPRETATION BETWEEN BOREHOLES</b></p> <p>----- SOUND TILLITE ROCK LEVEL</p> <p>----- SOIL-ROCK INTERFACE</p>
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## Appendix A: Borehole Logs

HOLE No: BH1  
Sheet 1 of 1

JOB: 3030041301

ROCK FABRIC: MF-massive, BF-bedded, FF-foliated, CF-cleaved, SF-schistose, GF-gneissose, LF-laminated  
 GRAIN SIZE: FG-fine grained, MG-medium grain, CG-coarse grain  
 JOINT SPACING: VCJ-very close spacg, CJ-close spacing, MJ-medium spacing, WJ-wide spacing, VWJ-very wide spacng  
 JOINT ROUGHNESS: SLJ-slickensided, SJ-smooth, RJ-rough  
 JOINT SHAPE: CUR-curvilinear, PLA-planar, UND-undulating, STE-stepped, IRR-irregular  
 ROCK HARDNESS: EHR-extremely hard rock, VHR-very hard rock, HR-hard rock, MHR-medium hard rock, SR-soft rock, VSR-very soft rock



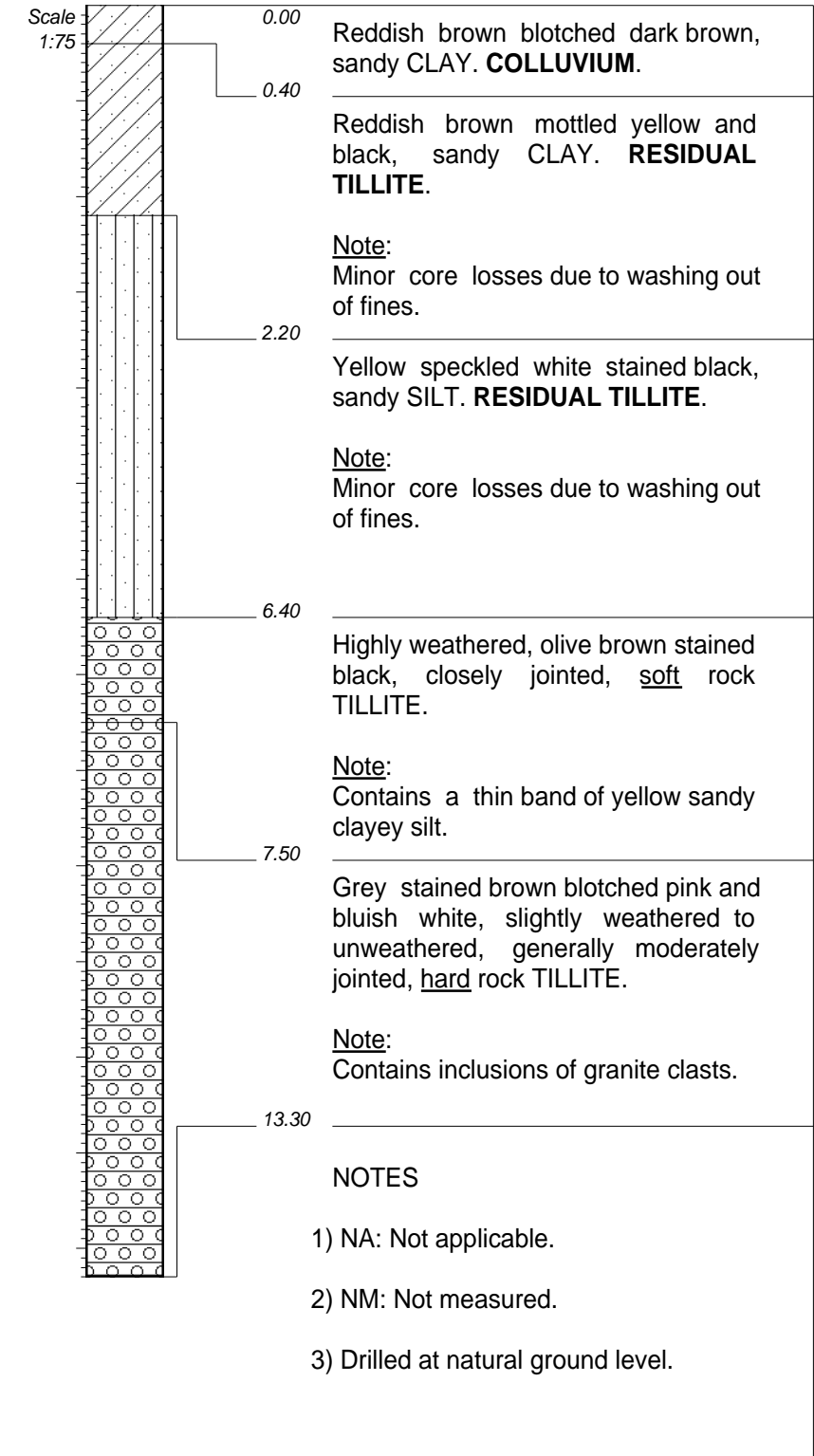
UMKHOMAZI PROJECT  
MAPSTONE DAM DRILLING INVESTIGATION

HOLE No: BH1  
Sheet 1 of 1

GEOTECHNICAL INVESTIGATION

JOB: 3030041301

Grain Size	Rock Fabric	Fabric Spac (mm)	Fabric Inc (deg)	Joint Set No.	Joint Inc (Deg)	Joint Spac	Micro Roughness	Joint Filling	Fill Thickness (mm)	Depth m	Mat recov %	Rock recov %	RQD %	Frac Freq No/m
NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	1,5	60	0	0	NA
NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	1,95	SPT	N=7		
NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	3	71	0	0	NA
NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	3,45	SPT	N=18		
NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	4,5	78	0	0	NA
NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	4,95	SPT	N=49		
NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	6	100	0	0	NA
NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	6,15	SPT	N=Ref		
FG	BF	-	-	0	70-90	MJ	RJ	Clayey Silt	40	7,5	95	82	37	6
				1	20-40	MJ	RJ	Stained	-					
				2	40-60	WJ	RJ	Stained	-					
FG	BF	-	-	0	70-90	MJ-WJ	RJ	Stained	-	9	100	100	77	6
				1	40-60	WJ	RJ	Stained	-	10,5	100	100	90	3
				2	20-40	VWJ	RJ	Stained	-	12	100	100	100	1
										13,3	100	100	91	2



CONTRACTOR : Diabor  
MACHINE :  
DRILLED BY :  
PROFILED BY : AvdM  
TYPE SET BY : EM  
SETUP FILE : KPBHCOO.SET

INCLINATION : 90 degrees  
DIAM :  
DATE : 18 Nov - 5 Dec 2014  
DATE : 8 Dec 2014  
DATE : 12/12/2014 09:05  
TEXT : ..P51\PROFILES\MJVAVDM.TXT

COORDINATE SYSTEM : WGS84 (Lo31)  
X-COORD : S29 47 16.7  
Y-COORD : E30 23 25.8

HOLE No: BH1

HOLE No: BH2  
Sheet 1 of 1

JOB: 3030041301

ROCK FABRIC  
MF -massive  
BF -bedded  
FF -foliated  
CF -cleaved  
SF -schistose  
GF -gneissose  
LF -laminated

GRAIN SIZE  
FG -fine grained  
MG -medium grain  
CG -coarse grain

JOINT SPACING  
VCJ-very close spacg  
CJ -close spacing  
MJ -medium spacing  
WJ -wide spacing  
VWJ-very wide spacng

JOINT ROUGHNESS  
SLJ-slickensided  
SJ -smooth  
RJ -rough

JOINT SHAPE  
CUR-curvilinear  
PLA-planar  
UND-undulating  
STE-stepped  
IRR-irregular

ROCK HARDNESS  
EHR-extremely hard rock  
VHR-very hard rock  
HR -hard rock  
MHR-medium hard rock  
SR -soft rock  
VSR-very soft rock



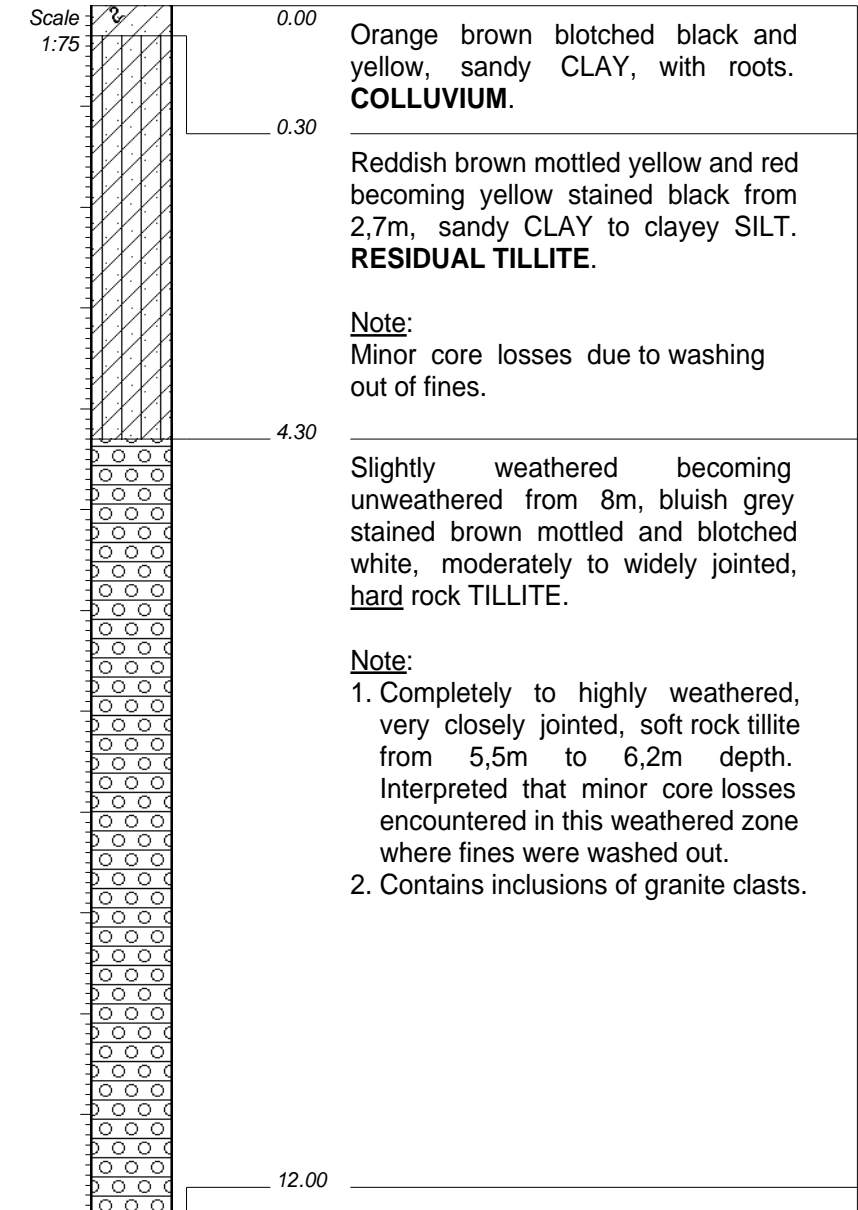
UMKHOMAZI PROJECT  
MAPSTONE DAM DRILLING INVESTIGATION

HOLE No: BH2  
Sheet 1 of 1

GEOTECHNICAL INVESTIGATION

JOB: 3030041301

Grain Size	Rock Fabric	Fabric Spac (mm)	Fabric Inc (deg)	Joint Set No.	Joint Inc (Deg)	Joint Spac	Micro Roughness	Joint Filling	Fill Thickness (mm)	Depth m	Mat recov %	Rock recov %	RQD %	Frac Freq No/m
NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	1,5	54	0	0	NA
NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	1,95	SPT	N=4		
NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	3	89	0	0	NA
NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	3,45	SPT	N=15		
NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	4,5	78	20	0	4
FG	BF	-	-	0 1 2	70-90 40-60 30-50	CJ-MJ WJ CJ	RJ RJ RJ	Stained - Stained silt	- - <2	6	88	88	51	7
										7,5	95	95	73	3
										9	100	100	87	1
										10,5	100	100	100	1
										12	100	100	100	-



NOTES

- 1) NA: Not applicable.
- 2) NM: Not measured.
- 3) Water depth of dam: 1,95m.

CONTRACTOR : Diabor  
MACHINE :  
DRILLED BY :  
PROFILED BY : AvdM  
TYPE SET BY : EM  
SETUP FILE : KPBHCOO.SET

INCLINATION : 90 degrees  
DIAM :  
DATE : 18 Nov - 5 Dec 2014  
DATE : 8 Dec 2014  
DATE : 12/12/2014 09:05  
TEXT : ..P51\PROFILES\MJVAVDM.TXT

COORDINATE SYSTEM : WGS84 (Lo31)  
X-COORD : S29 47 16.8  
Y-COORD : E30 23 27.1

HOLE No: BH2

HOLE No: BH3  
Sheet 1 of 1

JOB: 3030041301

ROCK FABRIC  
MF -massive  
BF -bedded  
FF -foliated  
CF -cleaved  
SF -schistose  
GF -gneissose  
LF -laminated

GRAIN SIZE  
FG -fine grained  
MG -medium grain  
CG -coarse grain

JOINT SPACING  
VCJ -very close spacg  
CJ -close spacing  
MJ -medium spacing  
WJ -wide spacing  
VWJ -very wide spacng

JOINT ROUGHNESS  
SLJ -slickensided  
SJ -smooth  
RJ -rough

JOINT SHAPE  
CUR -curvilinear  
PLA -planar  
UND -undulating  
STE -stepped  
IRR -irregular

ROCK HARDNESS  
EHR -extremely hard rock  
VHR -very hard rock  
HR -hard rock  
MHR -medium hard rock  
SR -soft rock  
VSR -very soft rock



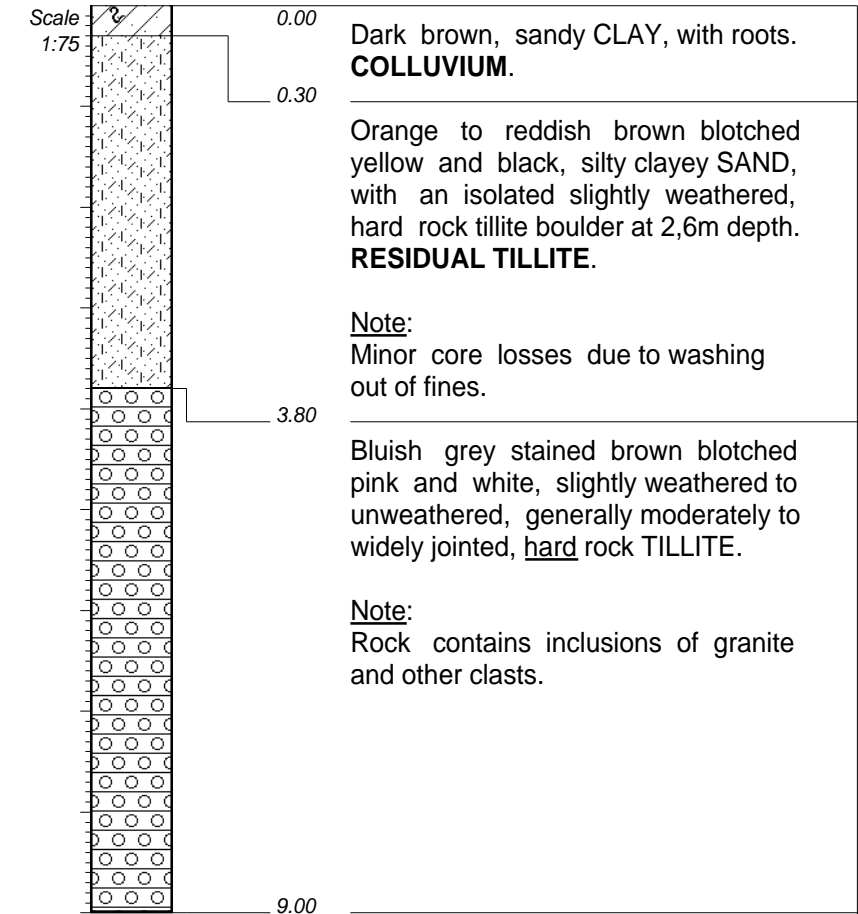
UMKHOMAZI PROJECT  
MAPSTONE DAM DRILLING INVESTIGATION

HOLE No: BH3  
Sheet 1 of 1

GEOTECHNICAL INVESTIGATION

JOB: 3030041301

Grain Size	Rock Fabric	Fabric Spac (mm)	Fabric Inc (deg)	Joint Set No.	Joint Inc (Deg)	Joint Spac	Micro Roughness	Joint Filling	Fill Thickness (mm)	Depth m	Mat recov %	Rock recov %	RQD %	Frac Freq No/m
NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	1,5	79	0	0	NA
NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	1,95	SPT	N=13		
NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	3	77	29	24	4
NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	3,9	74	52	52	2
FG	BF	-	-	0 1	70-90 50-70	MJ-WJ WJ	RJ RJ	Stained silt Stained silt	<2 <2	4,5	100	100	60	10
FG	BF	-	-	0 1	70-90 50-70	MJ-WJ WJ	RJ RJ	Stained silt Stained silt	<2 <2	6	100	100	78	5
FG	BF	-	-	0 1	70-90 50-70	MJ-WJ WJ	RJ RJ	Stained silt Stained silt	<2 <2	7,5	100	100	93	3
FG	BF	-	-	0 1	70-90 50-70	MJ-WJ WJ	RJ RJ	Stained silt Stained silt	<2 <2	9	100	100	100	1



NOTES

- 1) NA: Not applicable.
- 2) NM: Not measured.
- 3) Water depth of dam: 8m.

CONTRACTOR : Diabor  
MACHINE :  
DRILLED BY :  
PROFILED BY : AvdM  
TYPE SET BY : EM  
SETUP FILE : KPBHCOO.SET

INCLINATION : 90 degrees  
DIAM :  
DATE : 18 Nov - 5 Dec 2014  
DATE : 8 Dec 2014  
DATE : 12/12/2014 09:05  
TEXT : ..P51\PROFILES\MJ\VAVDM.TXT

COORDINATE SYSTEM : WGS84 (Lo31)  
X-COORD : S29 47 16.9  
Y-COORD : E30 23 28.2

HOLE No: BH3



HOLE No: BH4  
Sheet 1 of 1

JOB: 3030041301

<b>ROCK FABRIC</b>	<b>GRAIN SIZE</b>	<b>JOINT ROUGHNESS</b>	<b>ROCK HARDNESS</b>
MF -massive	FG -fine grained	SLJ-slickensided	EHR-extremely hard rock
BF -bedded	MG -medium grain	SJ -smooth	VHR-very hard rock
FF -foliated	CG -coarse grain	RJ -rough	HR -hard rock
CF -cleaved			MHR-medium hard rock
SF -schistose	<b>JOINT SPACING</b>	<b>JOINT SHAPE</b>	SR -soft rock
GF -gneissose	VCJ-very close spacg	CUR-curvilinear	VSR-very soft rock
LF -laminated	CJ -close spacing	PLA-planar	
	MJ -medium spacing	UND-undulating	
	WJ -wide spacing	STE-stepped	
	VWJ-very wide spacng	IRR-irregular	



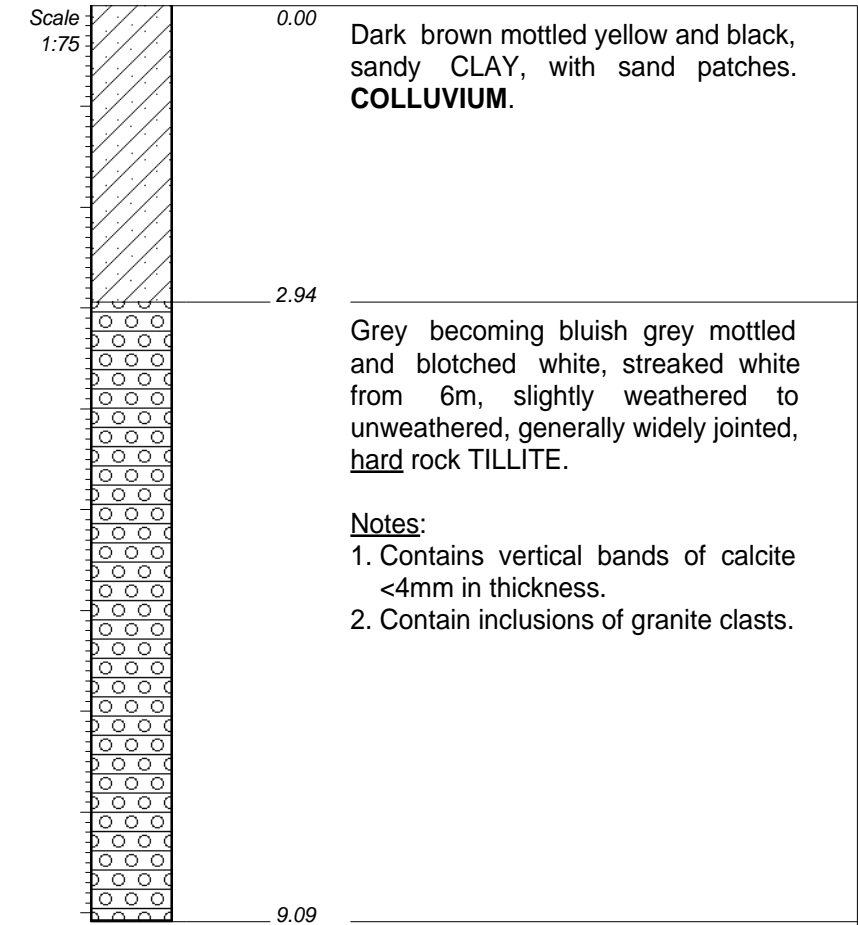
UMKHOMAZI PROJECT  
MAPSTONE DAM DRILLING INVESTIGATION

HOLE No: BH4  
Sheet 1 of 1

GEOTECHNICAL INVESTIGATION

JOB: 3030041301

Grain Size	Rock Fabric	Fabric Spac (mm)	Fabric Inc (deg)	Joint Set No.	Joint Inc (Deg)	Joint Spac	Micro Roughness	Joint Filling	Fill Thickness (mm)	Depth m	Mat recov %	Rock recov %	RQD %	Frac Freq No/m
NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	1,5	33	0	0	NA
										1,95	SPT	N=8		
										3	50	6	0	NA
FG	BF	-	-	0 1 2	70-90 30-50 40-60	MJ WJ WJ	RJ RJ RJ	Stained Calcite -	- <5 -	4,5	98	98	86	3
										5,52	100	100	100	2
										6,09	100	100	100	2
										7,59	100	100	100	1
										9,09	100	100	100	0



NOTES

- 1) NA: Not applicable.
- 2) NM: Not measured.
- 3) Water depth of dam: 3,85m.

CONTRACTOR : Diabor  
MACHINE :  
DRILLED BY :  
PROFILED BY : AvdM  
TYPE SET BY : EM  
SETUP FILE : KPBHCOO.SET

INCLINATION : 90 degrees  
DIAM :  
DATE : 18 Nov - 5 Dec 2014  
DATE : 8 Dec 2014

COORDINATE SYSTEM : WGS84 (Lo31)  
X-COORD : S29 47 16.9  
Y-COORD : E30 23 29.7

HOLE No: BH4

HOLE No: BH5  
Sheet 1 of 2

JOB: 3030041301

<b>ROCK FABRIC</b>	<b>GRAIN SIZE</b>	<b>JOINT ROUGHNESS</b>	<b>ROCK HARDNESS</b>
MF -massive	FG -fine grained	SLJ-slickensided	EHR-extremely hard rock
BF -bedded	MG -medium grain	SJ -smooth	VHR-very hard rock
FF -foliated	CG -coarse grain	RJ -rough	HR -hard rock
CF -cleaved			MHR-medium hard rock
SF -schistose	<b>JOINT SPACING</b>	<b>JOINT SHAPE</b>	SR -soft rock
GF -gneissose	VCJ-very close spacg	CUR-curvilinear	VSR-very soft rock
LF -laminated	CJ -close spacing	PLA-planar	
	MJ -medium spacing	UND-undulating	
	WJ -wide spacing	STE-stepped	
	VWJ-very wide spacng	IRR-irregular	



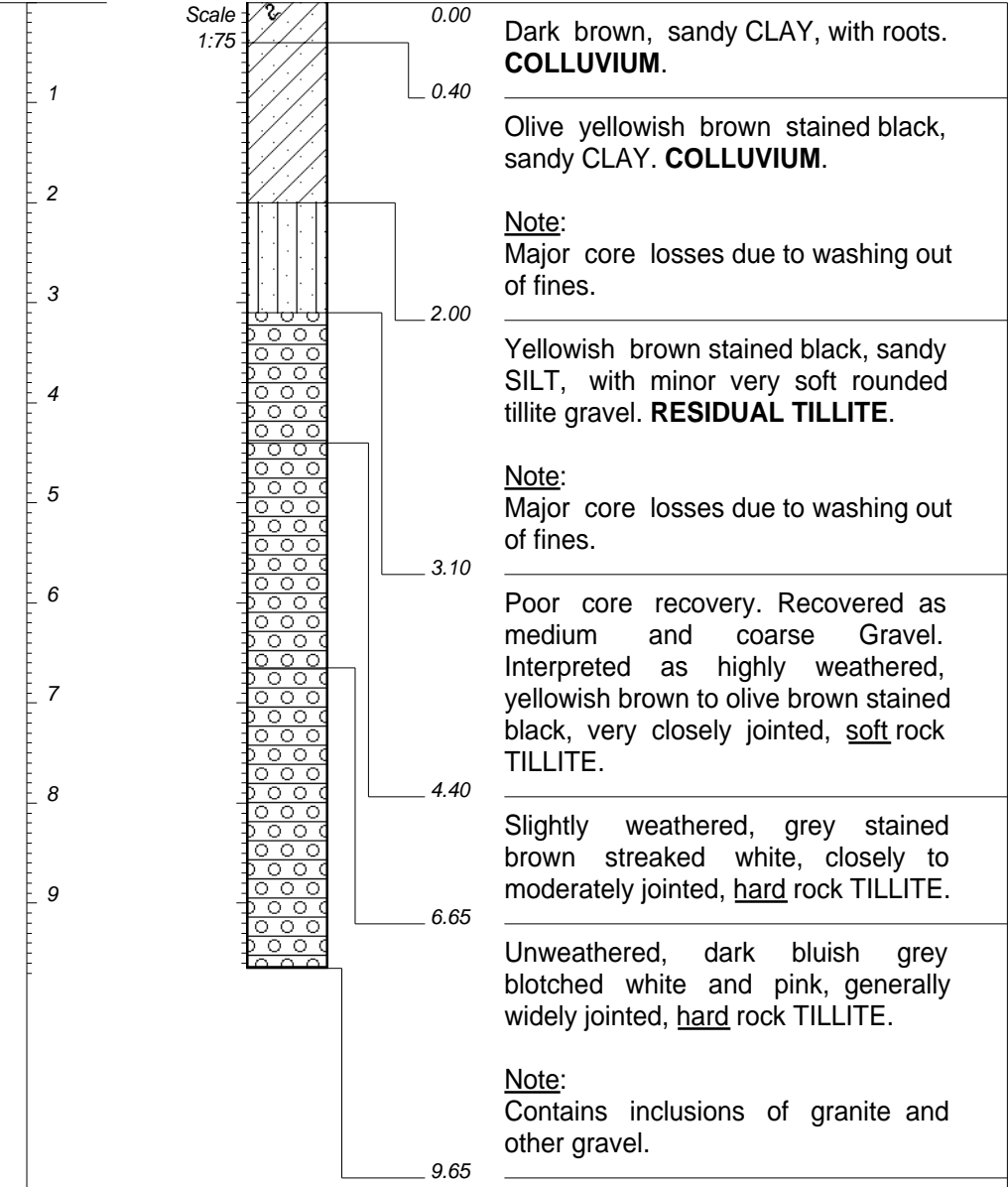
UMKHOMAZI PROJECT  
MAPSTONE DAM DRILLING INVESTIGATION

HOLE No: BH5  
Sheet 1 of 2

GEOTECHNICAL INVESTIGATION

JOB: 3030041301

Grain Size	Rock Fabric	Fabric Spac (mm)	Fabric Inc (deg)	Joint Set No.	Joint Inc (Deg)	Joint Spac	Micro Roughness	Joint Filling	Fill Thickness (mm)	Depth m	Mat recov %	Rock recov %	RQD %	Frac Freq No/m
NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	1,5	31	0	0	NA
NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	1,95	SPT	N=16		
NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	3	44	0	0	NA
FG	BF	-	-	NM	NM	NM	NM	NM	NM	4,5	42	7	0	NA
FG	BF	-	-	1	10-30	WJ	RJ	Stained	-	5,77	100	100	27	6
				2	30-40	MJ-WJ	RJ	Calcite	5					
				3	50-70	WJ	RJ	Stained	-					
FG	BF									6,95	100	100	81	3
FG	BF									8,45	100	100	100	1
										9,65	100	100	100	1



HOLE No: BH5  
Sheet 2 of 2

JOB: 3030041301

<b>ROCK FABRIC</b>	<b>GRAIN SIZE</b>	<b>JOINT ROUGHNESS</b>	<b>ROCK HARDNESS</b>
MF -massive	FG -fine grained	SLJ-slickensided	EHR-extremely hard rock
BF -bedded	MG -medium grain	SJ -smooth	VHR-very hard rock
FF -foliated	CG -coarse grain	RJ -rough	HR -hard rock
CF -cleaved			MHR-medium hard rock
SF -schistose	<b>JOINT SPACING</b>	<b>JOINT SHAPE</b>	SR -soft rock
GF -gneissose	VCJ-very close spacg	CUR-curvilinear	VSR-very soft rock
LF -laminated	CJ -close spacing	PLA-planar	
	MJ -medium spacing	UND-undulating	
	WJ -wide spacing	STE-stepped	
	VWJ-very wide spacng	IRR-irregular	



UMKHOMAZI PROJECT  
MAPSTONE DAM DRILLING INVESTIGATION

GEOTECHNICAL INVESTIGATION

HOLE No: BH5  
Sheet 2 of 2

JOB: 3030041301

NOTES

- 1) NA: Not applicable.
- 2) NM: Not measured.
- 3) Water depth of dam: 1,25m.

Grain Size	Rock Fabric	Fabric Spac (mm)	Fabric Inc (deg)	Joint Set No.	Joint Inc (Deg)	Joint Spac	Micro Roughness	Joint Filling	Fill Thickness (mm)	Depth m	Mat recov %	Rock recov %	RQD %	Frac Freq No/m	DEPTH Scale 1:75

CONTRACTOR : Diabor  
MACHINE :  
DRILLED BY :  
PROFILED BY : AvdM  
TYPE SET BY : EM  
SETUP FILE : KPBHCOO.SET

INCLINATION : 90 degrees  
DIAM :  
DATE : 18 Nov - 5 Dec 2014  
DATE : 8 Dec 2014

COORDINATE SYSTEM : WGS84 (Lo31)  
X-COORD : S29 47 16.8  
Y-COORD : E30 23 30.8

DATE : 12/12/2014 09:05  
TEXT : ..P51\PROFILES\MJVAVDM.TXT

HOLE No: BH5

# Appendix B: Borehole Core Photographs

## BH1



## BH2



BH3



BH4



BH5

